

Application Note

Characterization Methods for Flexible Absorber Sheets WE-FAS



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1 The Flexible Absorber Sheet WE-FAS

Electromagnetic Interference (EMI) has become a serious problem as it can occur anywhere in electronic circuits with unpredictable and detrimental effects. This issue has grown in recent years due to a number of factors including increases in device frequency, high integration in electronic systems, higher power densities and reductions in PCB thickness and size.

The most common means of solving electromagnetic noise problems is to shield the system with conductive materials such as shielded enclosures, foil tape or conductive gaskets. Nevertheless, a large number of electronic devices have many parts that operate at high frequencies that can cause complex EMI problems that cannot be removed with conductive shielding. In order to avoid these issues, Flexible Absorber Sheets, like the WE-FAS series, which is made of a polymer filled with ferrite powder material, can be used to suppress the unwanted high-frequency EM components.



Figure 1: WE-FAS Flexible Absorber Sheets

2 Absorber Sheet Properties

One of the most important parameters that describes the material's ability to absorb direct and dissipated electromagnetic noise is represented by the part μ'' of the complex permeability (μ). A material's permeability is the result of molecular composition and structure and is defined as the complex permeability. The real part quantifies the stored energy or inductive component while the imaginary part quantifies the absorbed energy or absorption component:

$$\mu_r = \mu_r' - j\mu_r'' \quad (\text{Eq. 1})$$

The behavior of these parameters depends on the material composition and is frequency dependent. Thus, it is very important to know in which frequency range noise levels exceed maximum permitted limits. With this data, it is possible to establish a balance between reflection and magnetic losses depending on the application and the kind of electromagnetic noise. Figure 2 shows the complex permeability of several flexible absorber sheets of WE FAS series with different performance characteristics.

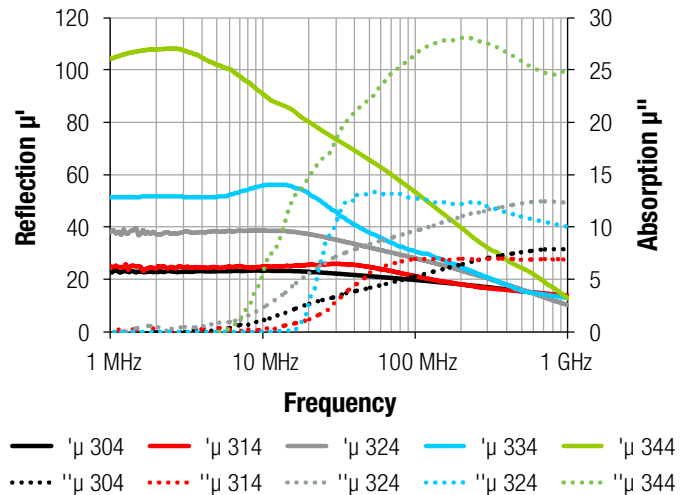


Figure 2: Permeability of flexible absorber sheet materials

As permeability is frequency dependent, the correct material need to be selected according to the frequency range where noise levels need to be suppressed. Standard specification don't give this information. As they only state general parameters instead of absorption and reflection components:

Part number	Thickness (mm)	$\mu'_{\text{typ}} @ 1\text{MHz}$	Dimensions (mm)
304 03S	0.3	23	330 x 210
304 05S	0.5	23	330 x 210
304 10S	1.0	23	330 x 210
314 01	0.1	25	297 x 210
314 02	0.2	25	297 x 210
314 03	0.3	25	297 x 210
324 01S	0.1	39	297 x 210
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324 03S	0.3	39	297 x 210
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324 075 S	0.75	39	297 x 210
324 10S	1.0	39	297 x 210
334 01	0.1	55	297 x 210
334 02	0.2	55	297 x 210
334 03	0.3	55	297 x 210
344 01	0.1	100	297 x 210
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Table 1: Overview of WE-FAS series

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Nevertheless, it can be difficult to estimate the absorber material performance as it is the result of a multitude of variables in addition to the absorber permeability. These include sheet thickness, size and geometry, as well as the distance between the noise source and absorber material. Thus, in basic systems the attenuation of a certain electromagnetic noise suppression material cannot be estimated. However, in order to study the effect in more complex electronic systems, it is often better to obtain real results through some experimental characterization techniques.

It is more interesting to measure the absorbing capacity through experimental setups that make it possible to evaluate the material performance of several sheets that demonstrate different behavior. Thereby, several experimental tests are described that can be used to characterize absorber materials based upon internal and external properties.

The characterization techniques described simulate specific problems focused on transmission lines, cavity resonance and magnetic decoupling. These setups and experimental results will be shown below in order to determine which material provides the best performance to reduce electromagnetic noise problems depending on the application.

3 Microstrip Line Method

This technique makes it possible to evaluate the performance of the flexible absorber sheets in systems with transmission line issues through an experimental procedure. In this way, several sheets with different composition or thickness can be tested in order to obtain the maximum transmission attenuation power ratio in a specific application.

These problems can appear in high-frequency data buses where digital signals switch in the frequency range of MHz or GHz that can produce conducted noise on the data lines. An interesting solution in this sort of application is to place an absorber sheet on the data bus as shown in Figure 3. This acts as a low-pass filter absorbing or attenuating high frequency conducted noise.

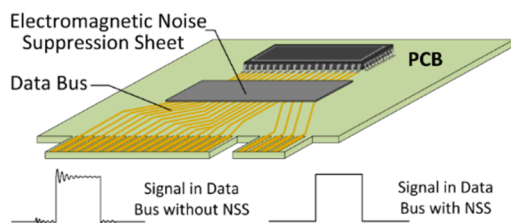


Figure 3: Transmission Line Application

A method based on a microstrip line (MSL) test fixture is used to evaluate the attenuation of conducting current noise in a PCB or noise path when the noise suppression sheet is in place. Thereby, the MSL is employed as a transmission line, whereby a noise signal will be measured to know the sample absorption ability. Hence, this test fixture simulates a noise source inside an electronic circuit and it is therefore possible to determine the transmission absorption.

The manufactured MSL employed in this procedure consists of a PCB where the strip conductor is printed and two SMA type connectors are connected in both ends. The MSL is composed of polytetrafluoroethylene (PTFE) dielectric PCB material (length = 100 mm, width = 50 mm, thickness = 1.6 mm), a copper strip conductor (length = 54.4 mm, width = 4.4 mm, thickness = 0.018 mm) and a copper ground plane located in the bottom (length = 100 mm, width = 50 mm, thickness = 0.018 mm). The SMA connectors are installed on the opposite side of the MSL and they are connected with the end of the MSL through two vias.

The absorbing ratio can be obtained by comparing the transmission line power ratio before and after installing the absorbing sheet on the test fixture. In order to carry out the measurements, each end of a network analyzer coaxial cable is connected to each SMA test fixture ports, as shown in Figure 4. The network analyzer has to be configured to operate as signal source and signal receiver through measuring the S21 parameters to start the measurement procedure.

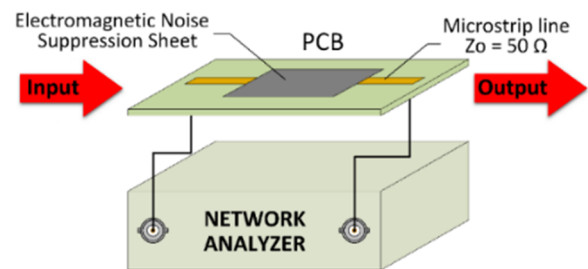


Figure 4: Microstrip Line Measurement System

The results presented in Figure 5 show all available materials in 0.3 mm thickness which have been measured with the microstrip line setup described above.

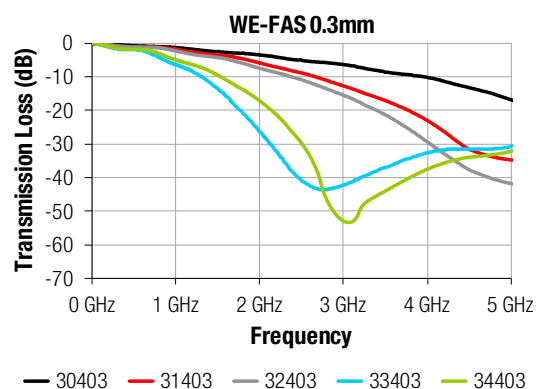


Figure 5: Transmission coefficient as a function of different materials

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In the [Appendix I](#) you will find further data acquired of different materials with different thickness of the [WE-FAS](#) range. Considering this, it is possible to evaluate the absorber materials performance according to their composition and thickness.

4 Coaxial Line Method

Coaxial line experimental method provides a means of studying the noise suppression capabilities of the material to solve resonant cavity EMI issues. Cavity resonance is a problem that can appear when an electronic circuit is placed inside a metal enclosure. Noisy circuits usually cause the resonance inside the enclosure, which may cause interference problems or even generate a system malfunction. Considering this, after evaluating some absorber materials with several compositions and sheet thickness, it is possible to choose the sheet with the best performance to filter the resonant frequency. In this kind of application, a sheet is placed under the cover of the metal enclosure to absorb the electromagnetic noise as illustrated in Figure 6. A means of reducing these issues is to place an absorber sheet inside the enclosure to attenuate or suppress the resonance by reducing the internal reflections. To evaluate this material in this kind of application, an experimental measurement system based on a coaxial line is utilized. In this procedure, one terminal of the coaxial line is shorted with a metallic surface, and the reflected energy inside it is measured with a network analyzer, as shown in Figure 7.

In order to characterize the absorption capacity of different compositions and/or thicknesses, it is necessary to repeat the process setting the absorber material attached over the reflector and compare the results. The evaluation of absorber materials in this experiment is carried out by measuring the reflection parameter (S11) with the reference value set as the coaxial line without the absorber material. Next, the sample is placed between the reflection material and a reflective material before the measurement is made. By comparing reference and measured data, it is possible to study the performance of each sheet. The reflection attenuation measured with the experimental coaxial line method as shown in Figure 8 with 0.3 mm thickness. Again, several

WE-FAS with different materials and thicknesses have been tested in the [Appendix II](#) in order to evaluate the attenuation ability in each case.

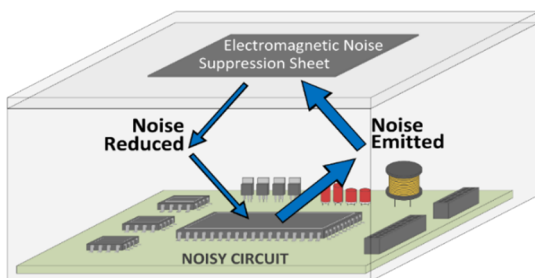


Figure 6: Coaxial Line Application

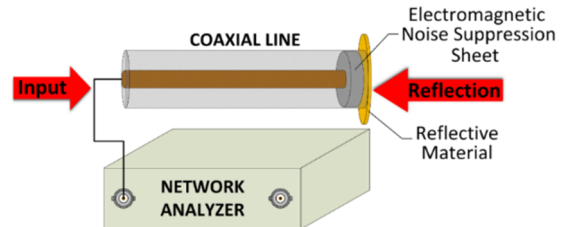


Figure 7: Coaxial Line Measurement Procedure

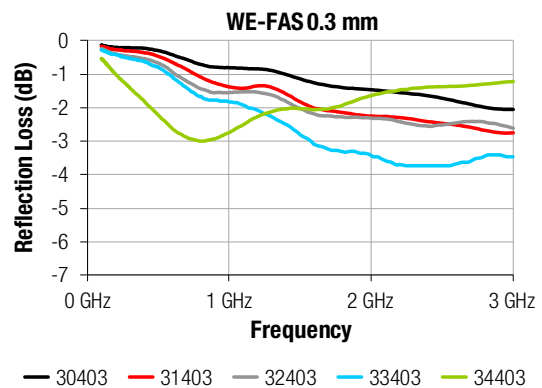


Abbildung 8: Reflexionsdämpfung als Funktion unterschiedlicher Materialien

5 Magnetic Decoupling Method

Magnetic decoupling is a common issue in electronic systems, which affects PCBs or devices with high-density layouts and circuits. This electromagnetic interference situation is often observed when there is a noisy electronic component or circuit placed on a PCB that can affect nearby elements and components. An interesting solution which can reduce the unintentional coupling of this kind is to focus on filtering the electromagnetic interference by placing the absorber sheet on the noise source or protecting the interfered part, as shown in Figure 9.

This technique analyzes the magnetic sheets absorption capacity for reducing or suppressing the coupling by employing a microstrip line test fixture to generate the EMI interference and a near field probe (NFP) to measure them. Thereby, this setup simulates a coupling system whereby one is used as a noise source and the other as a receiver or victim. The absorption effect is determined through connecting one port of the network analyzer to one terminal of the microstrip line and terminating the other connector with a load of 50 Ω . Subsequently, the NFP is placed perpendicular to the track and connected to the second port of the network analyzer, as shown in Figure 10. Subsequently, a network analyzer is configured as the signal source and signal receiver and the S21 parameters are compared before (reference) and after placing each absorber sheet on the microstrip line. The measured data with the absorber sample in place is subtracted from the reference.

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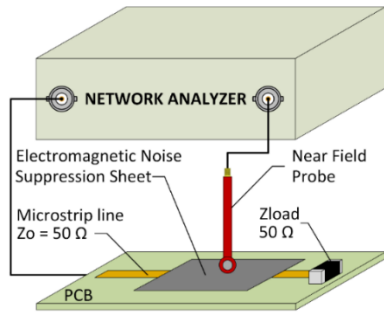


Figure 10: Magnetic Decoupling Measurement Technique

Data obtained through the magnetic decoupling technique is represented in Figure 11. The graph chart shows the measurement of WE-FAS with different material in 0.3 mm thickness. More graph charts in the [Appendix III](#) show the data also for different thicknesses.

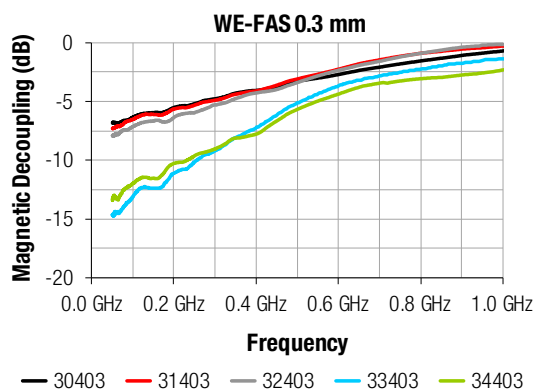


Figure 11: Magnetic Decoupling as a function of sheet materials

6 Summary

Taking everything into consideration, WE-FAS Flexible Absorber Sheets can solve a variety of EMI problems in different kinds of applications. Thereby, absorber materials have been characterized in order to be employed in applications with data buses affected by conducted problems, electronic circuits located inside an enclosure with malfunctions due to cavity resonance and electromagnetic interference between components placed in the same circuit or in close proximity to it.

Absorber sheets can provide several advantages in controlling EMI. This is confirmed with experimental techniques, which provide results in terms of attenuation ratio depending on the kind of problem therefore demonstrating the best option to use when solving a specific EMI problem. Furthermore, several thicknesses have been evaluated to demonstrate the performance of different products depending on the device space limits. Therefore, these materials can provide an innovative, straightforward solution without the need to modify or redesign the electronic circuit or product.

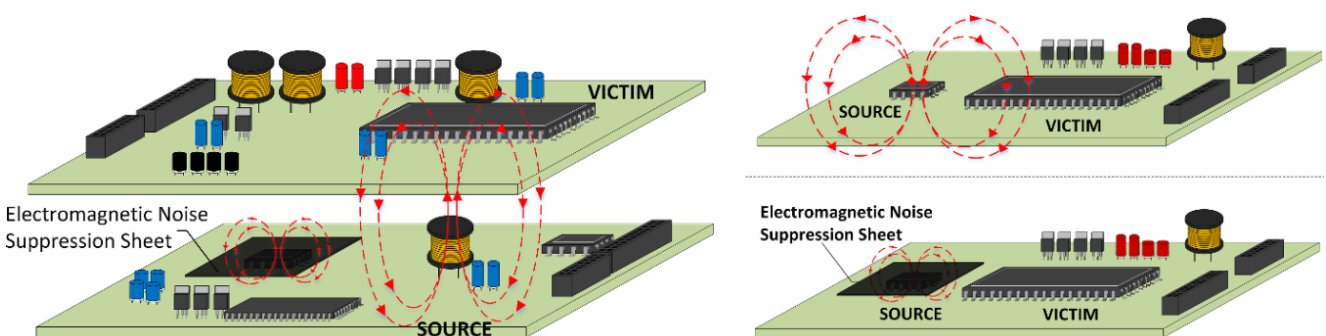


Figure 9: Magnetic Decoupling Applications

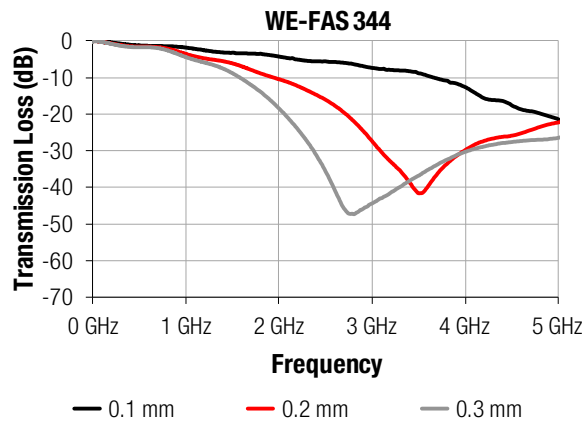
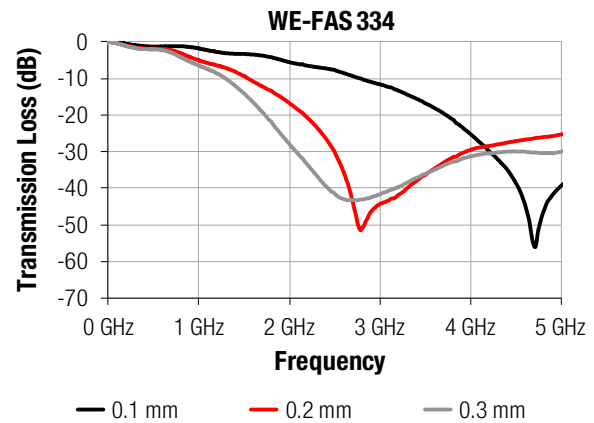
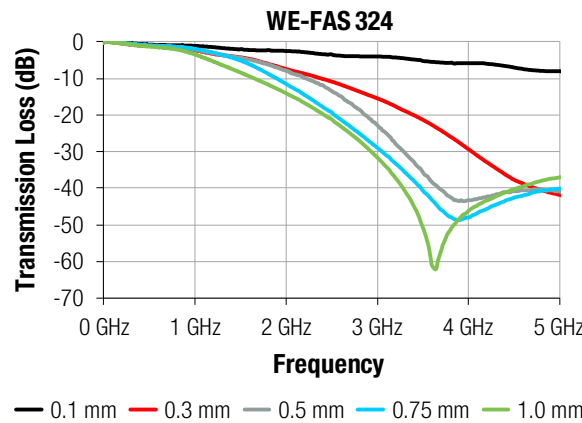
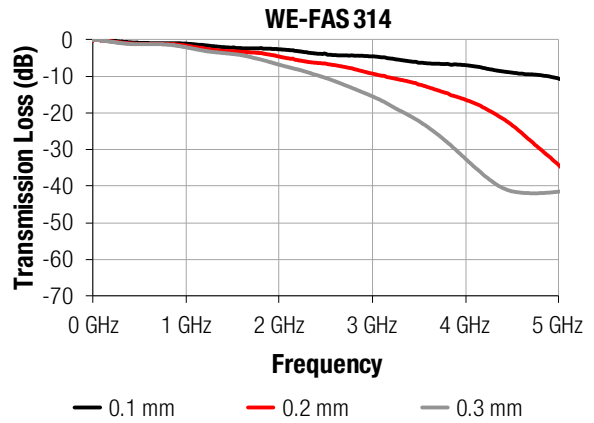
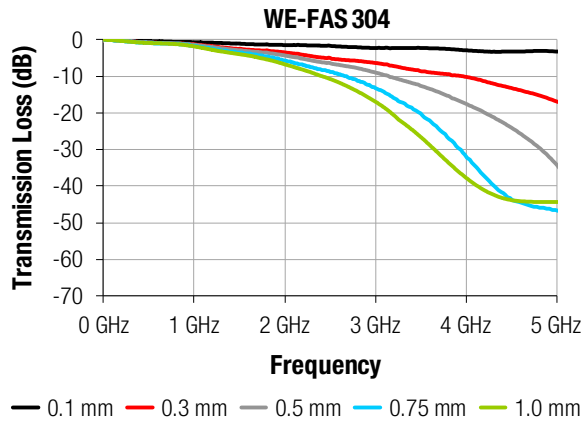
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A. Appendix

A.1. Appendix I - Transmission coefficient as a function of sheet thickness

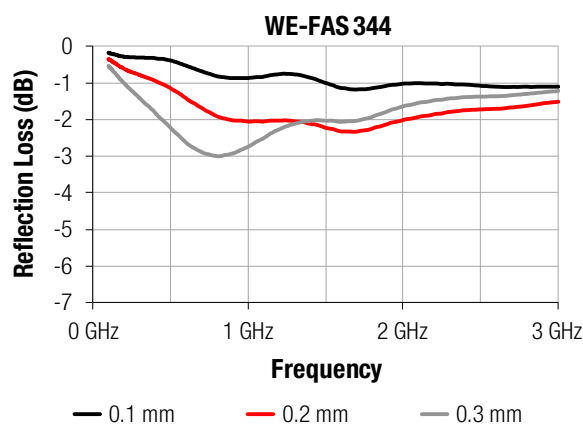
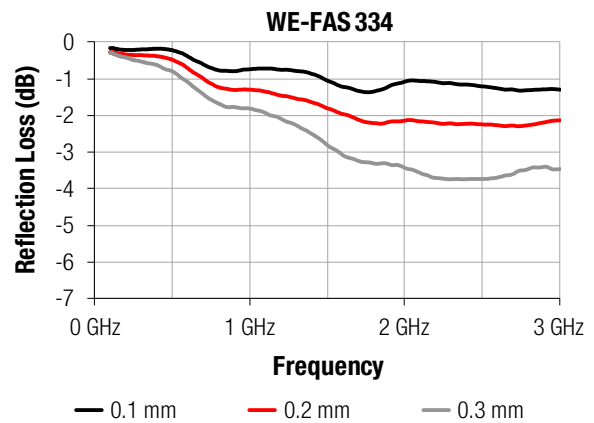
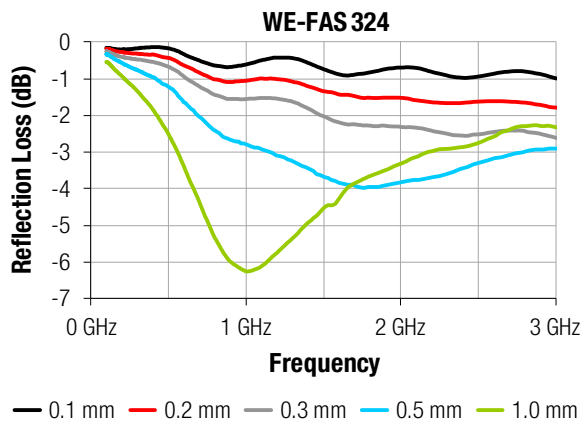
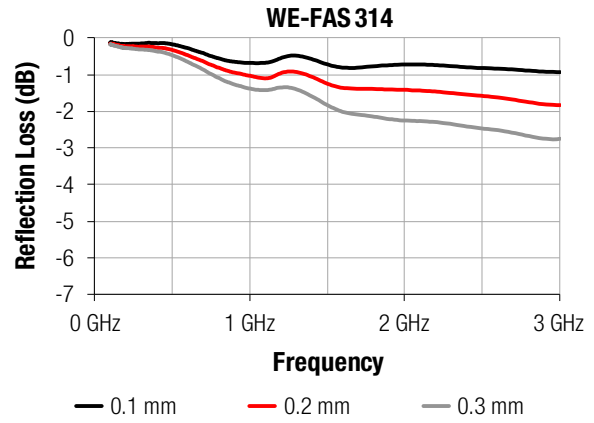
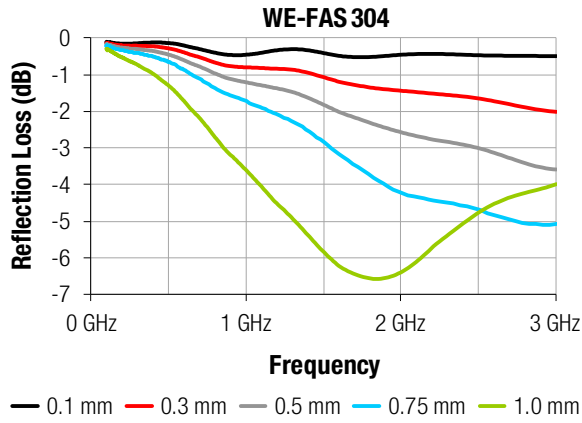


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A.2. Appendix II - Reflection coefficient as a function of sheet thickness

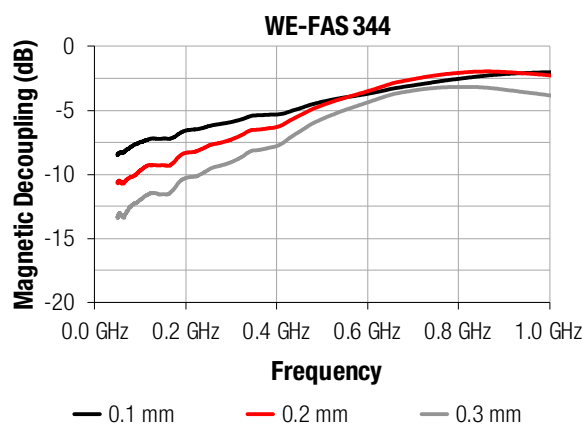
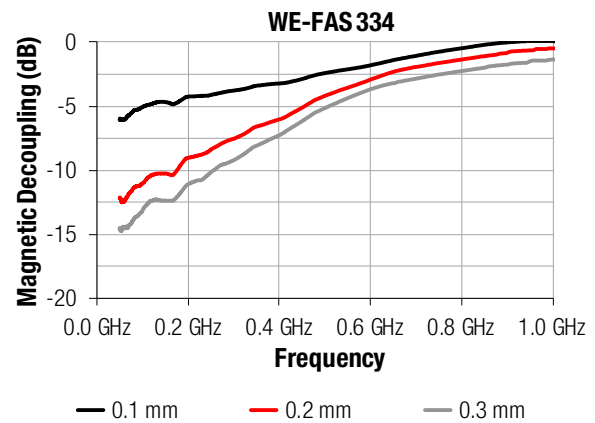
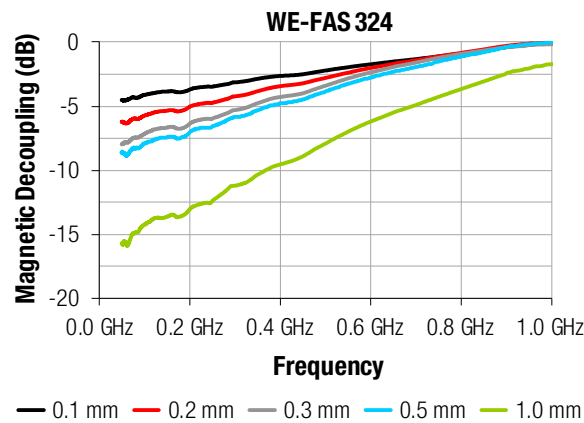
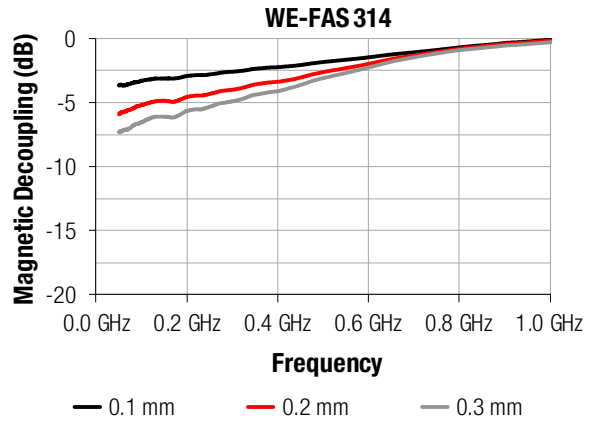
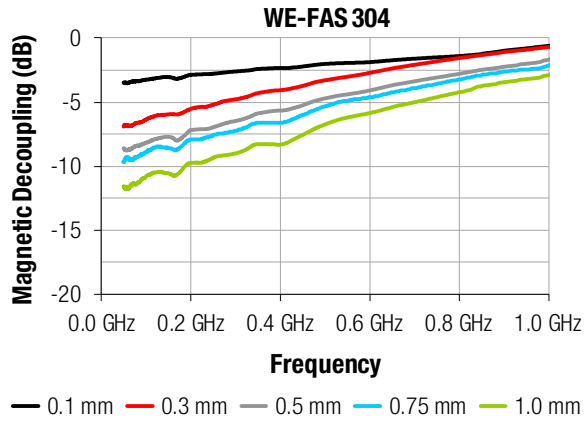


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A.3. Appendix III - Magnetic Decoupling as a function of sheet thickness



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A.4. Bill of Material

Part number	Thickness (mm)	$\mu'_{\text{typ}} @ 1\text{MHz}$	Dimensions (mm)
304 03S	0.3	23	330 x 210
304 05S	0.5	23	330 x 210
304 10S	1.0	23	330 x 210
314 01	0.1	25	297 x 210
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324 01S	0.1	39	297 x 210
324 02S	0.2	39	297 x 210
324 03S	0.3	39	297 x 210
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324 10S	1.0	39	297 x 210
334 01	0.1	55	297 x 210
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